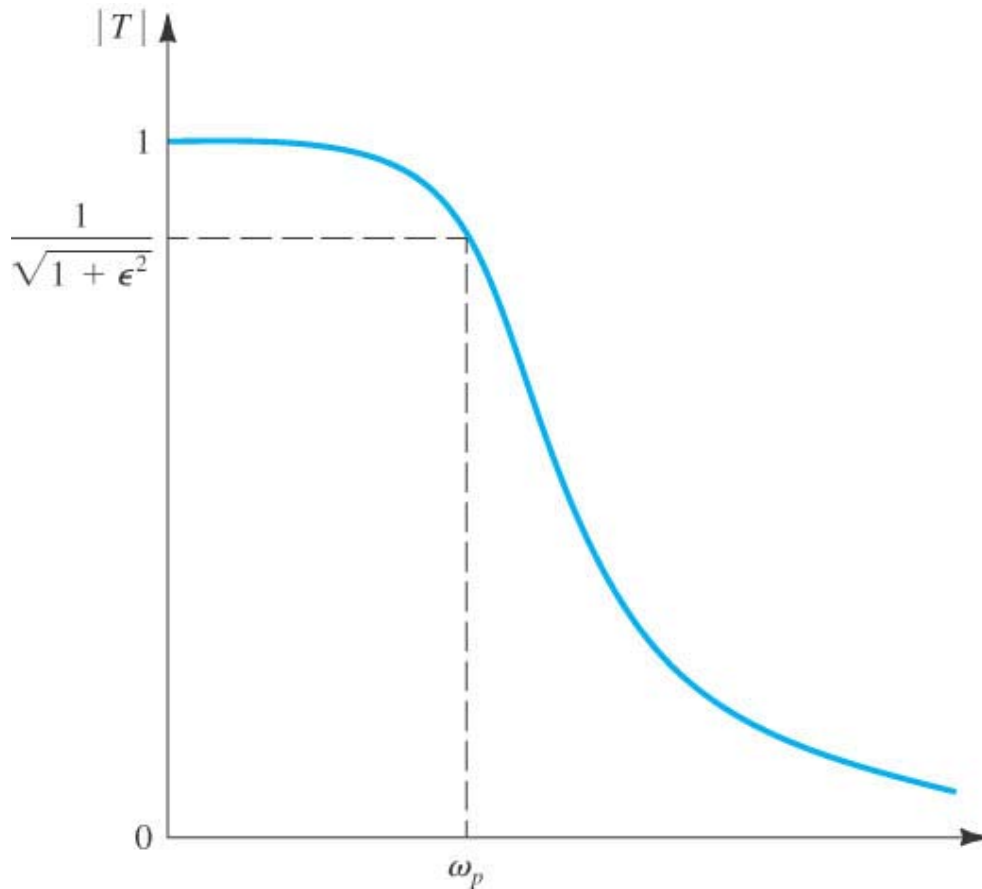


The Butterworth Filter



$$|T(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \left(\frac{\omega}{\omega_p}\right)^{2N}}}$$

$$|T(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2}} \text{ when } \omega = \omega_p$$

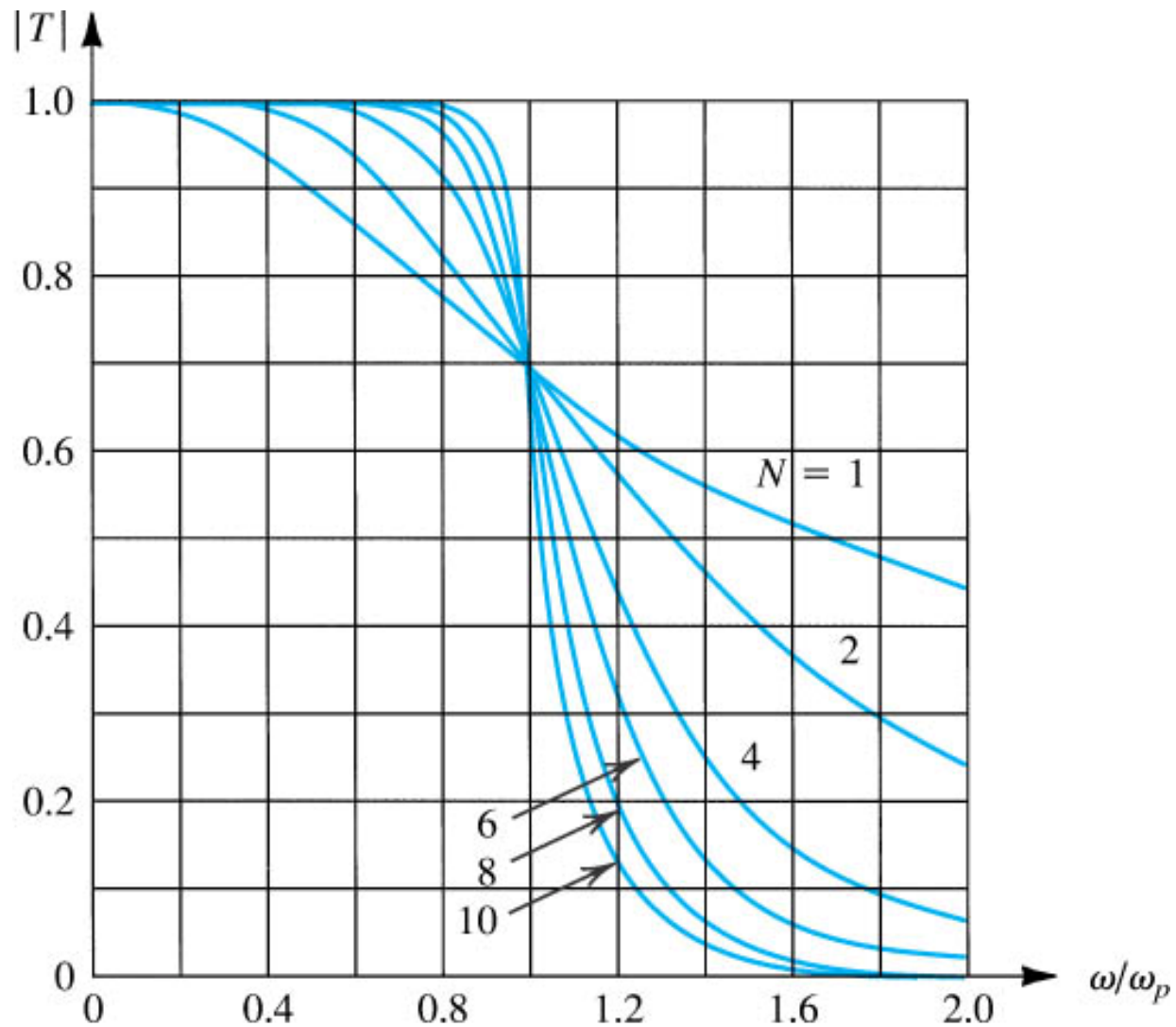
$$A_{\max} = 20 \log \sqrt{1 + \epsilon^2}$$

$$\epsilon = \sqrt{10^{A_{\max}/10} - 1}$$

$$A(\omega_s) = 10 \log[1 + \epsilon^2 (\omega_s / \omega_p)^{2N}]$$

$$T(s) = \frac{K \omega_0^N}{(s - p_1)(s - p_2) \dots (s - p_N)}$$

Magnitude response for Butterworth filters of various order

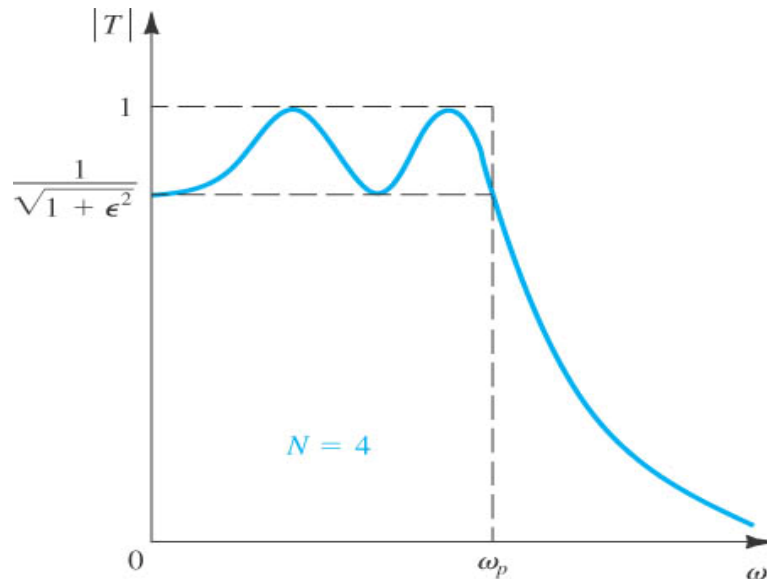


The Chebyshev Filter

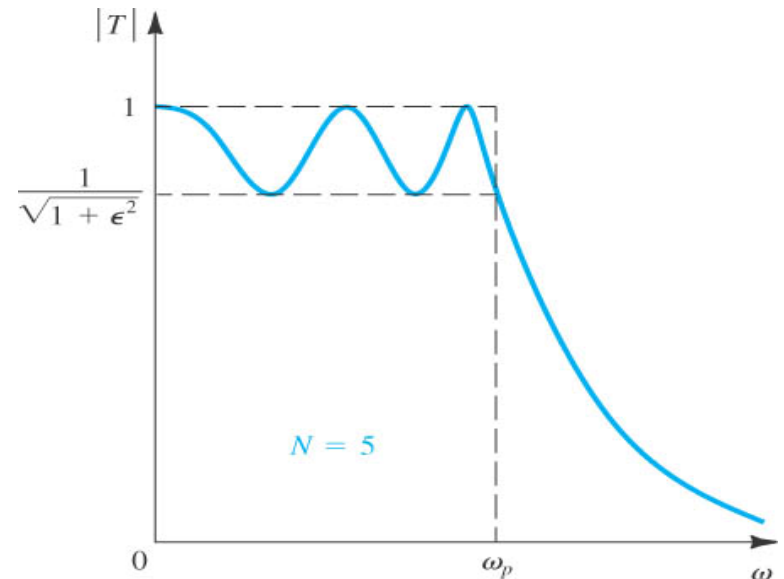
$$|T(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \cos^2[N \cos^{-1}(\omega/\omega_p)]}} \text{ for } \omega \leq \omega_p$$

$$|T(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2 \cosh^2[N \cosh^{-1}(\omega/\omega_p)]}} \text{ for } \omega \geq \omega_p$$

$$|T(j\omega)| = \frac{1}{\sqrt{1 + \epsilon^2}} \text{ when } \omega = \omega_p$$



(a)



(b)

$$A_{\max} = 10 \log(1 + \varepsilon^2)$$

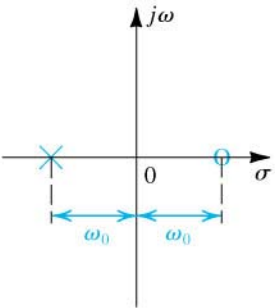
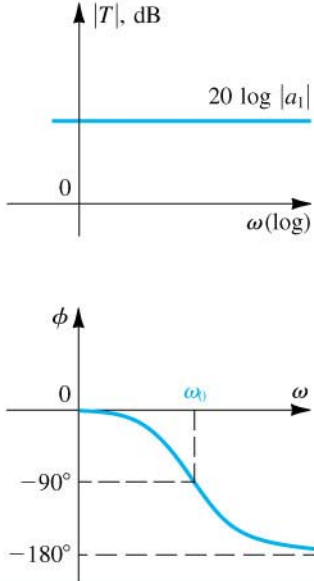
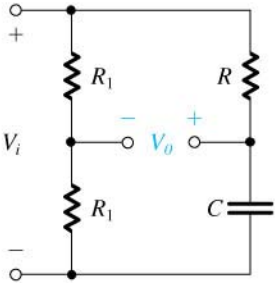
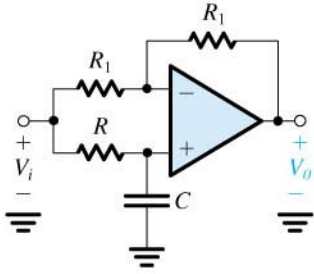
$$\varepsilon = \sqrt{10^{A_{\max} / 10} - 1}$$

$$A(\omega_s) = 10 \log[1 + \varepsilon^2 \cosh^2(N \cosh^{-1}(\omega_s / \omega_p))]$$

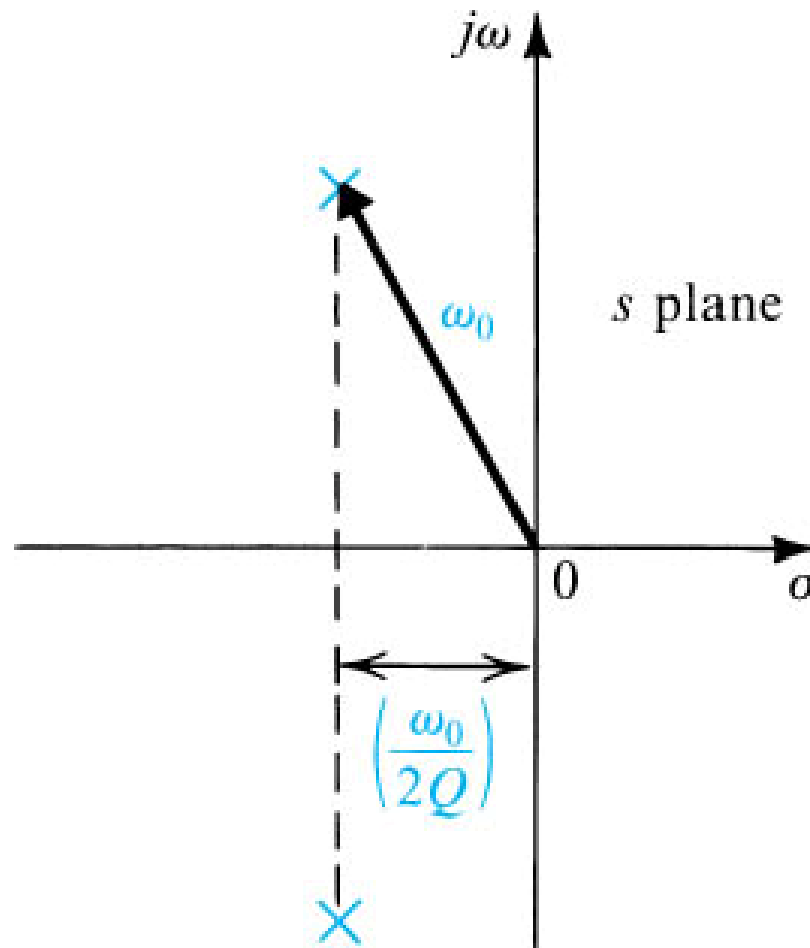
$$T(s) = \frac{K \omega_p^N}{\varepsilon 2^{N-1} (s - p_1)(s - p_2) \dots (s - p_N)}$$

First Order Filter Functions

Filter Type and $T(s)$	s-Plane Singularities	Bode Plot for $ T $	Passive Realization	Op Amp-RC Realization
(a) Low pass (LP) $T(s) = \frac{a_0}{s + \omega_0}$			$CR = \frac{1}{\omega_0}$ DC gain = 1	$CR_2 = \frac{1}{\omega_0}$ DC gain = $-\frac{R_2}{R_1}$
(b) High pass (HP) $T(s) = \frac{a_1 s}{s + \omega_0}$			$CR = \frac{1}{\omega_0}$ High-frequency gain = 1	$CR_1 = \frac{1}{\omega_0}$ High-frequency gain = $-\frac{R_2}{R_1}$
(c) General $T(s) = \frac{a_1 s + a_0}{s + \omega_0}$			$(C_1 + C_2)(R_1 \parallel R_2) = \frac{1}{\omega_0}$ $C_1 R_1 = \frac{a_1}{a_0}$ DC gain = $\frac{R_2}{R_1 + R_2}$ HF gain = $\frac{C_1}{C_1 + C_2}$	$C_2 R_2 = \frac{1}{\omega_0}$ $C_1 R_1 = \frac{a_1}{a_0}$ DC gain = $-\frac{R_2}{R_1}$ HF gain = $-\frac{C_1}{C_2}$

$T(s)$	Singularities	$ T $ and ϕ	Passive Realization	Op Amp-RC Realization
All pass (AP) $T(s) = -a_1 \frac{s - \omega_0}{s + \omega_0}$ $a_1 > 0$			 $CR = 1/\omega_0$ Flat gain (a_1) = 0.5	 $CR = 1/\omega_0$ Flat gain (a_1) = 1

Second Order Filter Functions



Filter Type and $T(s)$	s-Plane Singularities	$ T $
(a) Low pass (LP) $T(s) = \frac{a_0}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ DC gain = $\frac{a_0}{\omega_0^2}$		
(b) High pass (HP) $T(s) = \frac{a_2 s^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ High-frequency gain = a_2		
(c) Bandpass (BP) $T(s) = \frac{a_1 s}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ Center-frequency gain = $\frac{a_1 Q}{\omega_0}$		

Filter Type and $T(s)$	s-Plane Singularities	$ T $
(d) Notch $T(s) = a_2 \frac{s^2 + \omega_0^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ DC gain = High-frequency gain = a_2		
(e) Low-pass notch (LPN) $T(s) = a_2 \frac{s^2 + \omega_n^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ $\omega_n \geq \omega_0$ DC gain = $a_2 \frac{\omega_n^2}{\omega_0^2}$ High-frequency gain = a_2		$\omega_{\max} = \omega_0 \sqrt{\frac{\left(\frac{\omega_n^2}{\omega_0^2}\right)\left(1 - \frac{1}{2Q^2}\right) - 1}{\frac{\omega_n^2}{\omega_0^2} + \frac{1}{2Q^2} - 1}}$
(f) High-pass notch (HPN) $T(s) = a_2 \frac{s^2 + \omega_n^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$ $\omega_n \leq \omega_0$ DC gain = $a_2 \frac{\omega_n^2}{\omega_0^2}$ High-frequency gain = a_2		$T_{\max} = \frac{ a_2 \frac{ \omega_n^2 - \omega_{\max}^2 }{\sqrt{(\omega_0^2 - \omega_{\max}^2)^2 + \left(\frac{\omega_0}{Q}\right)^2 \omega_{\max}^2}}}{ a_2 }$

(g) All pass (AP)

$$T(s) = a_2 \frac{s^2 - s\frac{\omega_0}{Q} + \omega_0^2}{s^2 + s\frac{\omega_0}{Q} + \omega_0^2}$$

Flat gain = a_2

