

## ELG 3331: A Tutorial for Chapter 8

### Problem 8.13

a. The circuit is non-inverting amplifier, and

$$v_o = \left(1 + \frac{R_F}{R_2}\right)v_S$$

b. Accordingly

$$v_o = \left(1 + \frac{220}{1.8}\right)v_S = 2.464 + 0.1232 \cos(\omega t) \text{ V}$$

### Problem 8.14

$$v_o = v_S$$

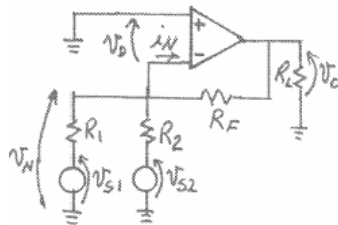
### Problem 8.17

The operational amplifier has a very input resistance, a very large open loop gain ( $\mu$ ), and a very small output resistance. Accordingly, it can be modeled with small error as an ideal operational amplifier.

Use KVL:

$$v_D + v_N = 0$$

$$v_D = 0, v_N = 0$$



Use KCL:

$$i_N + \frac{v_N - v_{S2}}{R_2} + \frac{v_N - v_{S1}}{R_1} + \frac{v_N - v_o}{R_F} = 0$$

$$v_N = 0$$

$$i_N = 0$$

$$v_o = -\frac{R_F}{R_1}v_{S1} - \frac{R_F}{R_2}v_{S2} = \left(-\frac{2.2}{0.85}\right)(7 \text{ mV}) + \left(-\frac{2.2}{1.5}\right)(7 \text{ mV}) = -28.38 \text{ mV}$$

Use the above results:  $A_{v1} = -2.588$  and  $A_{v2} = -1.467$

### Problem 8.40

The circuit is for low-pass filter.

$$V_o(j\omega) = -\frac{R_2}{R_1} \frac{1}{1 + j\omega CR_2} V_S(j\omega)$$

b.

$$H(j\omega) = \frac{V_o(j\omega)}{V_i(j\omega)} = -\frac{R_2}{R_1} \frac{1}{1 + j\omega CR_2}$$

c. The gain in decibel is obtained by

$$|H(j0)|_{dB} = 20 \log \frac{R_2}{R_1} = 20 \log \frac{22}{9.1} = 7.66 \text{ dB}$$

The cutoff frequency is

$$\omega_o = \frac{1}{CR_2} = \frac{1}{0.47 \times 10^{-6} \times 22 \times 10^3} = 96.71 \text{ rad/s}$$

### Problem 8.41

The amplifier is low-pass filter.

$$H(j\omega) = \frac{V_o(j\omega)}{V_i(j\omega)} = -\frac{R_2}{R_1} \frac{1}{1 + j\omega CR_2}$$

The gain in decibel is obtained by evaluating  $|H(j\omega)|$  at  $\omega = 0$ . For example

$$20 \log \frac{R_2}{R_1} = 20 \log \frac{68}{2.2} = 29.8 \text{ dB}$$

The cutoff frequency is

$$\omega_o = \frac{1}{CR_2} = \frac{1}{0.47 \times 10^{-9} \times 68 \times 10^3} = 31289 \text{ rad/s}$$