

MP10.1

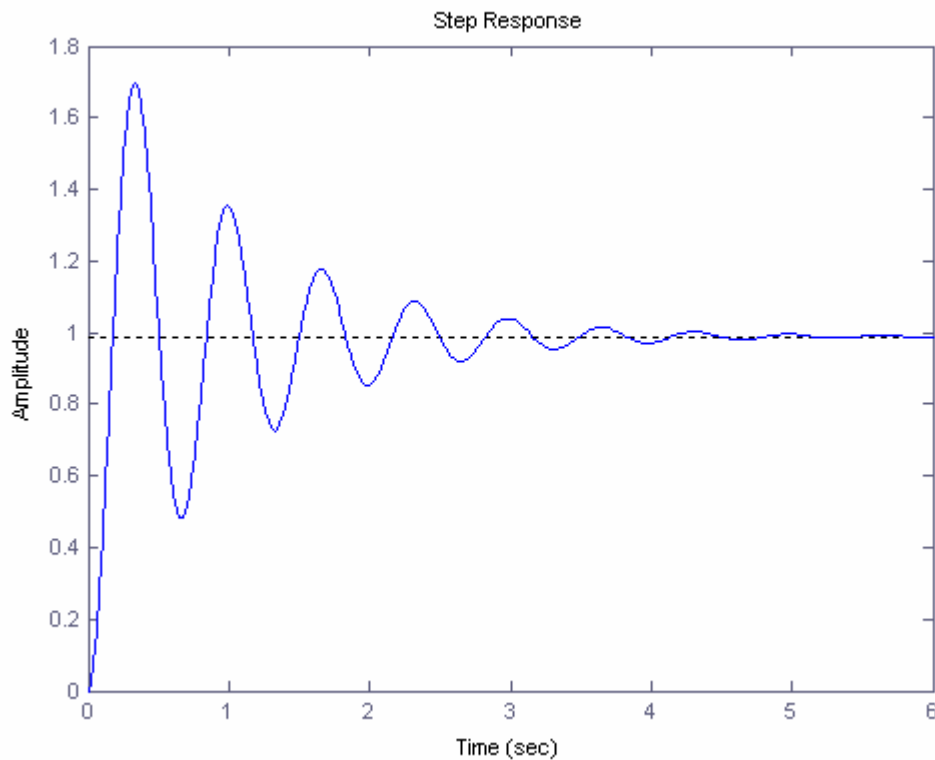
----- Code -----

```
numc=[10];denc=[1 1]; sysc=tf(numc,denc);  
numg=[9];deng=[1 1]; sysg=tf(numg,deng);  
sys=series(sysc, sysg);  
[mag, phase, w]=bode(sys);  
[gm, pm]=margin(mag, phase, w);  
pm
```

```
sys_cl=feedback(sys, [1]);  
y=step(sys_cl);  
step(sys_cl);  
ymax=max(y)
```

----- Result Shown -----

```
pm = 12.1343  
ymax = 1.6985
```



MP10.6

The settling time and phase margin specifications require that the dominant closed-loop poles have natural frequency and damping of $\omega_n \geq 1.78$ and $\zeta \geq 0.45$. The uncompensated roots locus is shown below

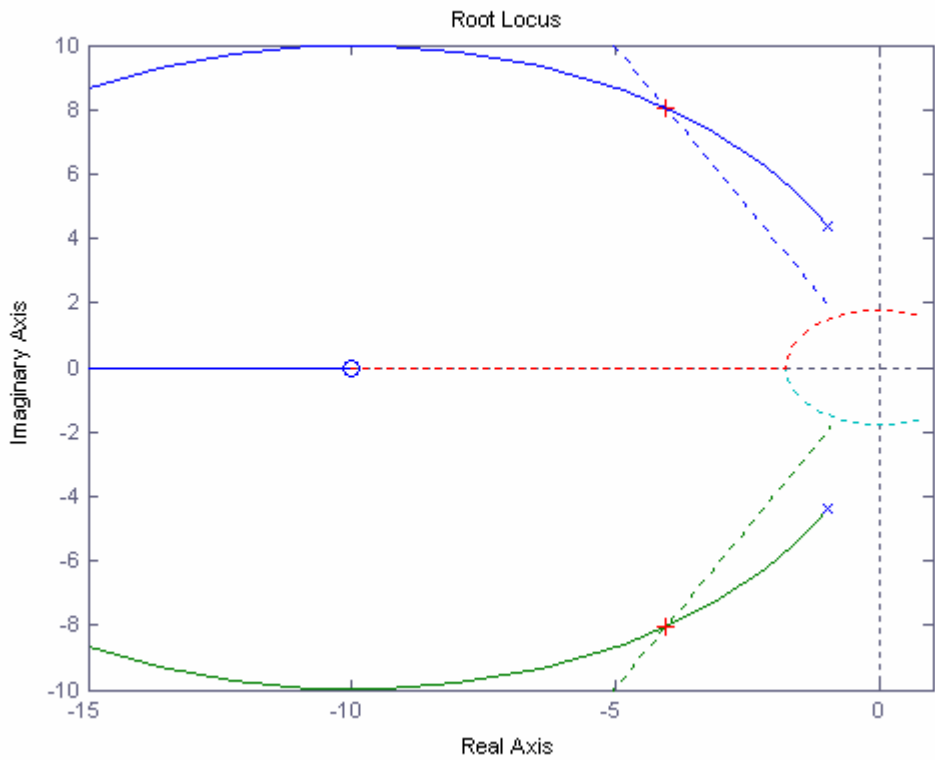
----- Code 1-----

```

numg=[1 10]; deng=[1 2 20]; sysg=tf(numg, deng);
rlocus(sysg);
axis([-15, 1, -10, 10]);
hold on
zeta=0.45; wn=1.7778;
x=[-10:0.1:-zeta*wn];
y=-(sqrt(1-zeta^2)/zeta)*x;
xc=[-10:0.1:zeta*wn];
c=sqrt(wn^2-xc.^2);
plot(x,y,'!',x,-y,'!',xc,c,'!',xc,-c,'!')
rlocfind(sysg),
hold off

```

----- Results -----
selected_point = -4.0616 + 8.0435i
ans = 6.1210



From the final value theorem, we determine that

$$K_p(\text{comp}) \geq 9$$

With the compensator

$$G_c(s) = K \frac{s+z}{s+p}$$

we find that

$$K_p(\text{comp}) = K \cdot (z/p) \cdot K_p(\text{uncomp})$$

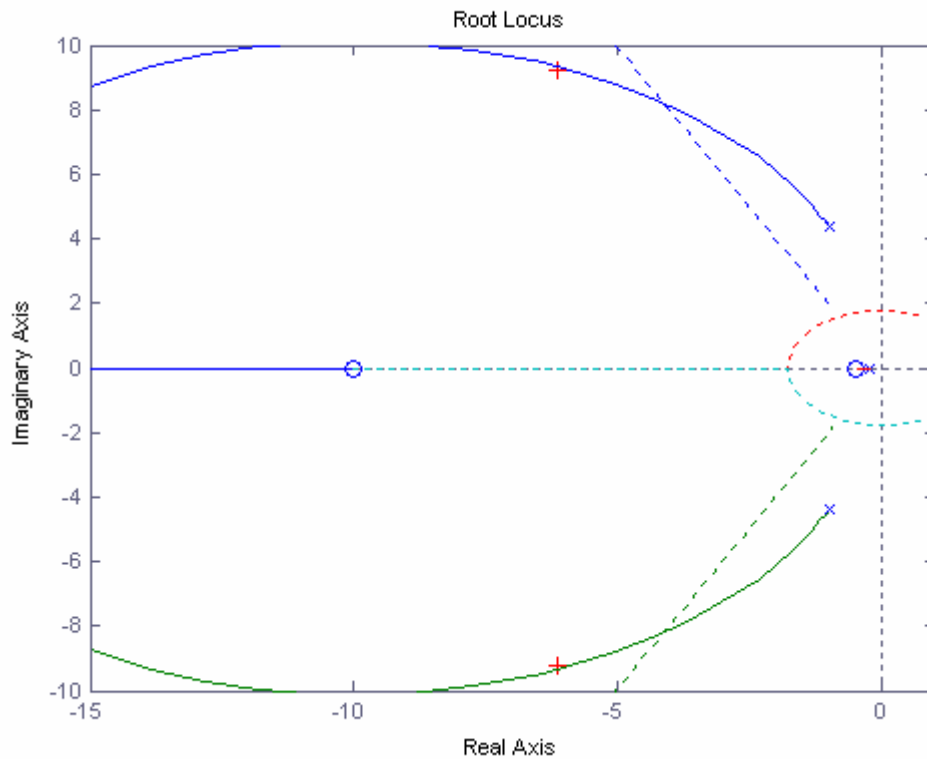
But $K_p(\text{uncomp}) = 0.5$ and a gain of $K = 10$ results in roots of the characteristic equation in the desired region. Solving for

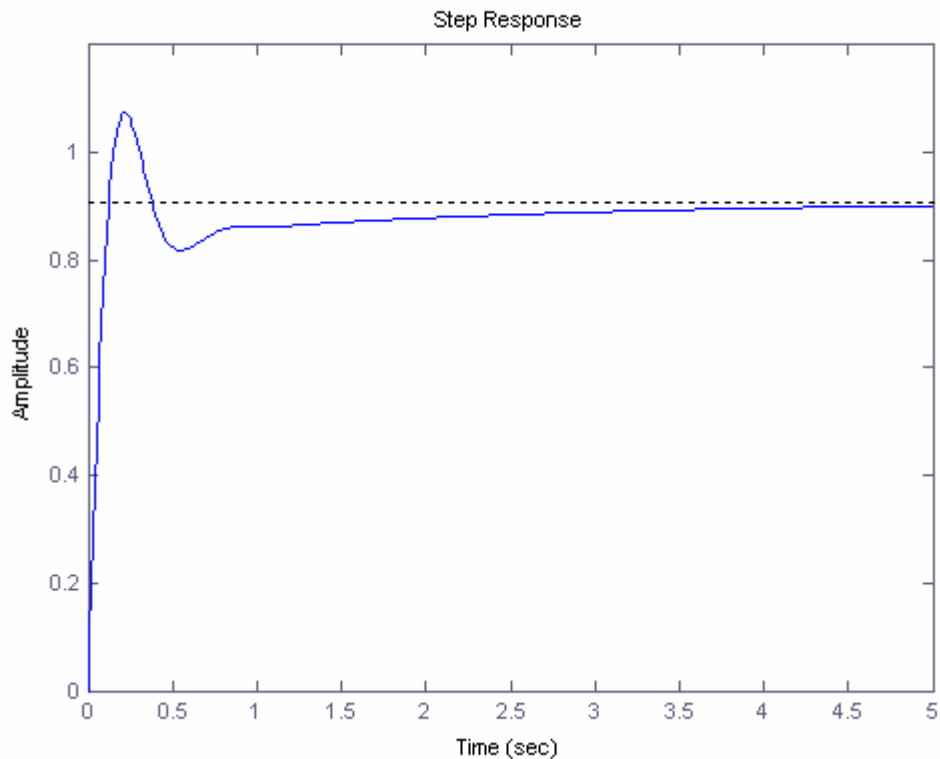
$$z/p = 1 \cdot K_p(\text{comp}) / (K \cdot K_p(\text{uncomp})) = 2.$$

Select $z = 0.5$ to minimize changing the root locus. Then, $p = 0.25$, and the compensator is

$$G_c(s) = 10 \frac{s+0.5}{s+0.25}$$

The compensated root locus and step response are shown below. The phase margin of the compensated system is P.M. = 62.3 degree and the settling time is less than 5 seconds.





----- Code 2-----

```

numg=[1 10]; deng=[1 2 20]; sysg=tf(numg, deng);
numc=[1 0.5]; denc=[1 0.25]; sysc=tf(numc, denc);
sys_o=series(sysc, sysg)
rlocus(sys_o);
axis([-15, 1, -10, 10]);
hold on
zeta=0.45; wn=1.7778;
x=[-10:0.1:-zeta*wn];
y=-(sqrt(1-zeta^2)/zeta)*x;
xc=[-10:0.1:zeta*wn];
c=sqrt(wn^2-xc.^2);
plot(x,y,'!',x,-y,'!',xc,c,'!',xc,-c,'!')
rlocfind(sysg)
hold off

```

----- Code 3-----

```

numg=[1 10]; deng=[1 2 20]; sysg=tf(numg, deng);
numc=10*[1 0.5]; denc=[1 0.25]; sysc=tf(numc, denc);
sys_o=series(sysc, sysg)
sys_cl=feedback(sys_o, [1])
t=[0:0.01:5]; step(sys_cl,t);
bode(sys_o), grid
[Gm,Pm]=margin(sys_o);
PmMax=max(Pm)

```

----- Results -----

PmMax = 62.0985

MP10.7

Both design specifications can be satisfied with an integral controller

$$G_c(s) = K_1 + \frac{K_2}{s} = \frac{10}{s}$$

----- Code -----

```
K1=0; K2=10;
numc=[K1, K2]; denc=[1 0]; sysc=tf(numc,denc);
numg=[23]; deng=[1 23]; sysg=tf(numg, deng);
sys_o=series(sysc, sysg)
sys_cl=feedback(sys_o, [1])
t=[0:0.01:1]; u=t;
subplot(211)
step(sys_cl,t), grid
subplot(212)
yr=lsim(sys_cl,u,t);
plot(t,yr(:)-u(:))
xlabel('Time (sec)'), ylabel('Tracking error')
title('Unit Ramp Response'), grid
```

