

ELG4172 Digital Signal Processing

- Tutorial #2

Presented by: Hitham Jleed



Discrete-Time Fourier Transform DTFT

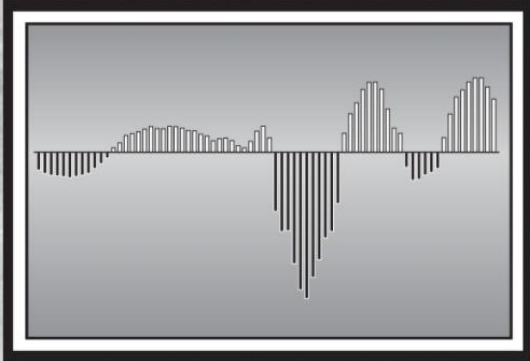
2 Discrete-Time Sign...

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Discrete-Time Signals and Systems



Review Discrete-Time Fourier Transform

$$X(e^{j\omega}) = \sum_{n=-\infty}^{\infty} x[n]e^{-j\omega n}$$

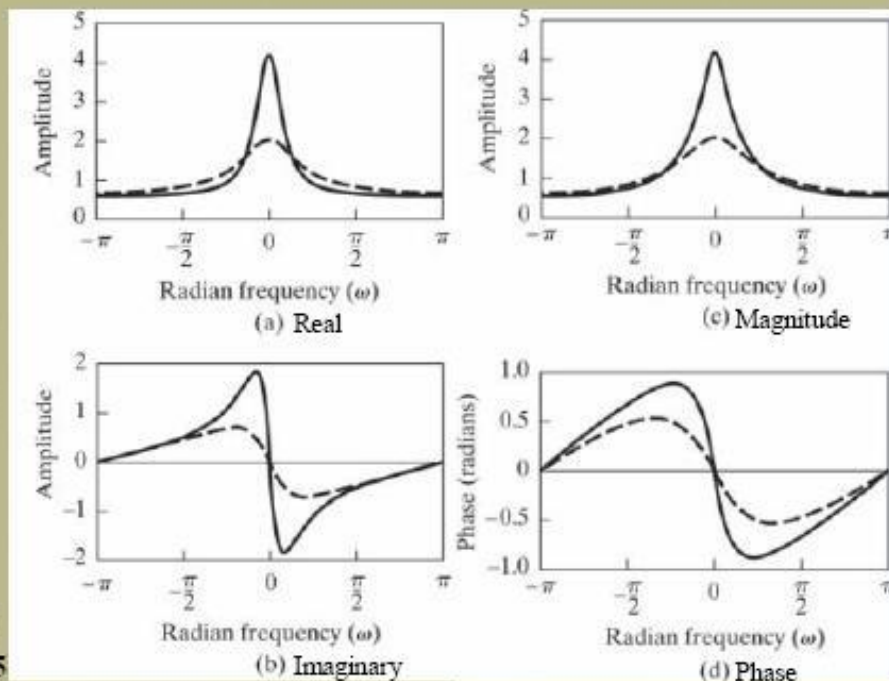
Fourier Transform

$$x[n] = \frac{1}{2\pi} \int_{2\pi} X(e^{j\omega})e^{j\omega n} d\omega,$$

Inverse Fourier Transform

◎ Signal $x[n] = a^n u[n]$

- Fourier transform $X(e^{j\omega}) = \frac{1}{1 - ae^{-j\omega}}$, if $|a| < 1$



Solid curve: $a=0.75$
Dashed curve: $a=0.5$

- 2.6. (a)** Determine the frequency response $H(e^{j\omega})$ of the LTI system whose input and output satisfy the difference equation

$$y[n] - \frac{1}{2}y[n-1] = x[n] + 2x[n-1] + x[n-2].$$

- (b)** Write a difference equation that characterizes a system whose frequency response is

$$H(e^{j\omega}) = \frac{1 - \frac{1}{2}e^{-j\omega} + e^{-j3\omega}}{1 + \frac{1}{2}e^{-j\omega} + \frac{3}{4}e^{-j2\omega}}.$$

2.6. (a) Determine the frequency response $H(e^{j\omega})$ of the LTI system whose input and output satisfy the difference equation

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(a) The difference equation:

$$y[n] - \frac{1}{2}y[n-1] = x[n] + 2x[n-1] + x[n-2]$$

Taking the Fourier transform of both sides,

$$Y(e^{j\omega})[1 - \frac{1}{2}e^{-j\omega}] = X(e^{j\omega})[1 + 2e^{-j\omega} + e^{-j2\omega}].$$

Hence, the frequency response is

$$H(e^{j\omega}) = \frac{Y(e^{j\omega})}{X(e^{j\omega})} = \frac{1 + 2e^{-j\omega} + e^{-j2\omega}}{1 - \frac{1}{2}e^{-j\omega}}.$$

(b) A system with frequency response:

$$H(e^{j\omega}) = \frac{Y(e^{j\omega})}{X(e^{j\omega})} = \frac{1 - \frac{1}{2}e^{-j\omega} + e^{-j3\omega}}{1 + \frac{1}{2}e^{-j\omega} + \frac{3}{4}e^{-j2\omega}}$$

cross multiplying,

$$Y(e^{j\omega})[1 + \frac{1}{2}e^{-j\omega} + \frac{3}{4}e^{-j2\omega}] = X(e^{j\omega})[1 - \frac{1}{2}e^{-j\omega} + e^{-j3\omega}],$$

and the inverse transform gives

$$y[n] + \frac{1}{2}y[n-1] + \frac{3}{4}y[n-2] = x[n] - \frac{1}{2}x[n-1] + x[n-3].$$

A linear time-invariant system is described by the following difference equation:

$$y(n) = ay(n-1) + bx(n), \quad 0 < a < 1$$

- (a) Determine the magnitude and phase of the frequency response $H(e^{j\omega})$ of the system.
- (b) Choose the parameter b so that the maximum value of $|H(e^{j\omega})|$ is unity, and sketch $|H(e^{j\omega})|$ and $\angle H(e^{j\omega})$ for $a = 0.9$.
- (c) Determine the output of the system to the input signal

$$x(n) = 5 + 12 \sin \frac{\pi}{2}n - 20 \cos \left(\pi n + \frac{\pi}{4} \right)$$

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$$x(n) = 5 + 12 \sin \frac{\pi}{2}n - 20 \cos \left(\pi n + \frac{\pi}{4} \right)$$

(a) The frequency response is

$$H(e^{j\omega}) = \frac{Y(e^{j\omega})}{X(e^{j\omega})} = \frac{b}{1 - ae^{-j\omega}}$$

Since

$$1 - ae^{-j\omega} = (1 - a \cos \omega) + ja \sin \omega$$

it follows that

$$\begin{aligned} |1 - ae^{-j\omega}| &= \sqrt{(1 - a \cos \omega)^2 + (a \sin \omega)^2} \\ &= \sqrt{1 + a^2 - 2a \cos \omega} \end{aligned}$$

$$|H(e^{j\omega})| = \frac{|b|}{|1 - ae^{-j\omega}|} = \frac{|b|}{\sqrt{1 + a^2 - 2a \cos \omega}}$$

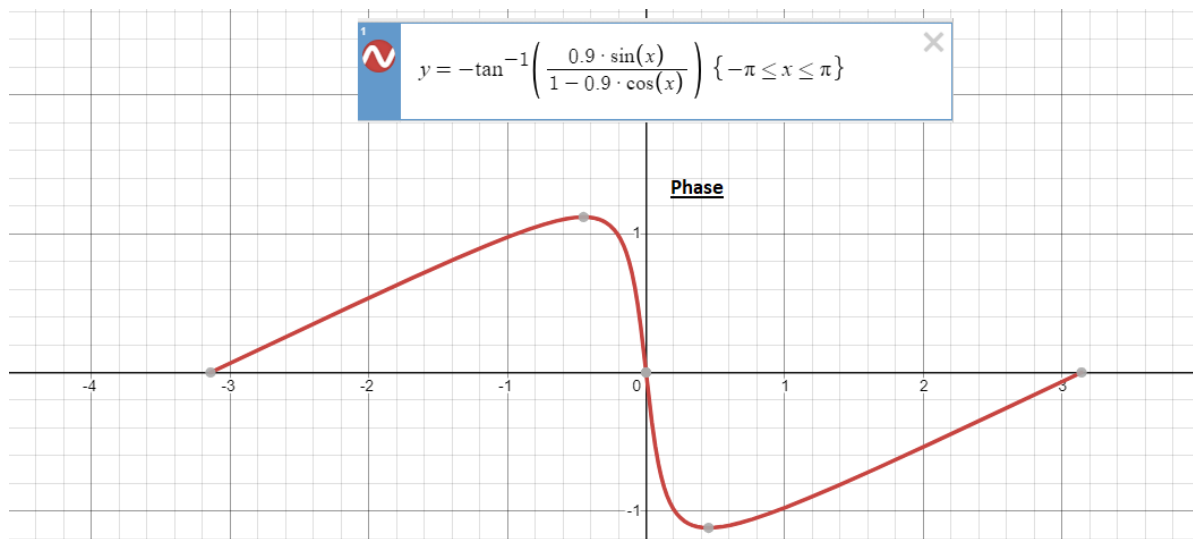
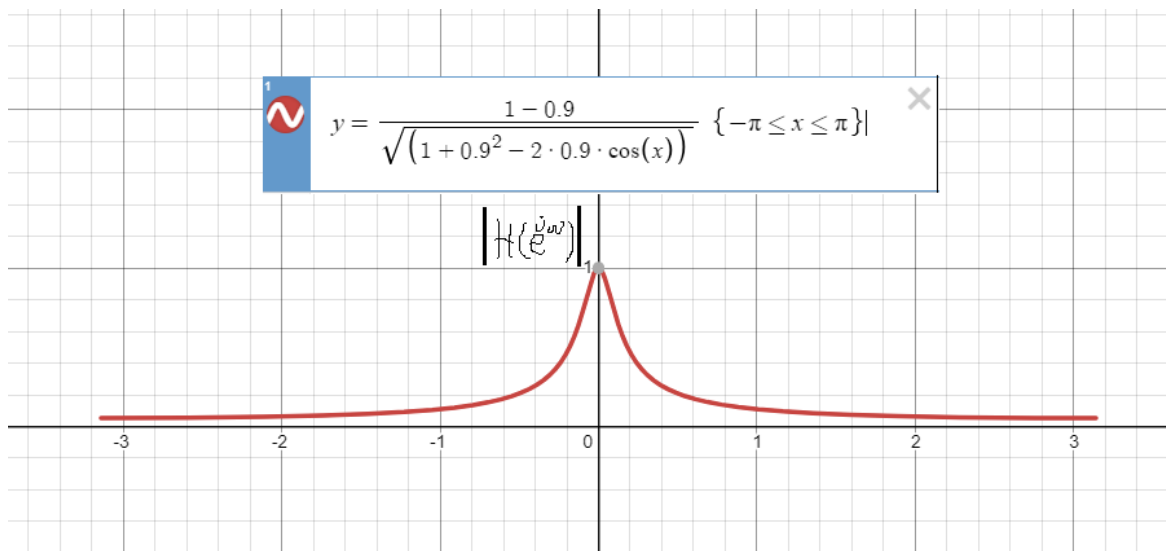
$$\angle H(e^{j\omega}) = \Theta(e^{j\omega}) = \angle b - \tan^{-1} \frac{a \sin \omega}{1 - a \cos \omega}$$

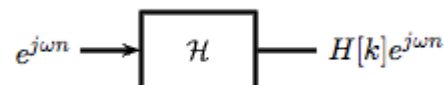
(b) Since the parameter a is positive, the denominator of $|H(e^{j\omega})|$ attains a minimum at $\omega = 0$. Therefore, $|H(e^{j\omega})|$ attains its maximum value at $\omega = 0$. At this frequency we have,

$$|H(0)| = \frac{|b|}{1 - a} = 1$$

which implies that $b = \pm(1 - a)$. We choose $b = 1 - a$, so that

$$|H(e^{j\omega})| = \frac{1 - a}{\sqrt{1 + a^2 - 2a \cos \omega}} \quad \text{and} \quad \Theta(e^{j\omega}) = -\tan^{-1} \frac{a \sin \omega}{1 - a \cos \omega}$$





(c) The input signal consists of components at frequencies $\omega = 0, \pi/2$, and π

For $\omega = 0$, $\Rightarrow |H(e^{j\omega})| = 1$ and $\Theta(0) = 0$. For $\omega = \pi/2$,

$$\omega = \pi/2 \quad \Rightarrow \quad |H(e^{j\omega})| = \frac{1-a}{\sqrt{1+a^2}} = \frac{0.1}{\sqrt{1.81}} = 0.074$$

$$\Theta\left(\frac{\pi}{2}\right) = -\tan^{-1} a = -42^\circ$$

$$\text{For } \omega = \pi, \quad \Rightarrow \quad |H(e^{j\omega})| = \frac{1-a}{1+a} = \frac{0.1}{1.9} = 0.053$$

$$\Theta(\pi) = 0$$

Therefore, the output of the system is

$$y(n) = 5|H(0)| + 12 \left| H\left(\frac{\pi}{2}\right) \right| \sin \left[\frac{\pi}{2}n + \Theta\left(\frac{\pi}{2}\right) \right] - 20|H(\pi)| \cos \left[\pi n + \frac{\pi}{4} + \Theta(\pi) \right]$$

8. An LTI system has impulse response $h[n] = 5(-1/2)^n u[n]$. Use the Fourier transform to find the output of this system when the input is $x[n] = (1/3)^n u[n]$.

Q 2.8

$$y[n] = h[n] * x[n]$$

FT $\left\{ \begin{array}{l} Y(e^{j\omega}) = H(e^{j\omega}) X(e^{j\omega}) \end{array} \right.$

$$H(e^{j\omega}) = \frac{5}{1 + \frac{1}{2} e^{-j\omega}}$$

$$X(e^{j\omega}) = \frac{1}{1 - \frac{1}{3} e^{-j\omega}}$$

$$Y(e^{j\omega}) = \frac{5}{1 + \frac{1}{2} e^{-j\omega}} \cdot \frac{1}{1 - \frac{1}{3} e^{-j\omega}}$$

$$= \frac{3}{1 + \frac{1}{2} e^{-j\omega}} + \frac{2}{1 - \frac{1}{3} e^{-j\omega}}$$

$$y[n] = 2\left(\frac{1}{3}\right)^n u[n] + 3\left(-\frac{1}{2}\right)^n u[n]$$

2.9. Consider the difference equation

$$y[n] - \frac{5}{6}y[n-1] + \frac{1}{6}y[n-2] = \frac{1}{3}x[n-1].$$

(a) What are the impulse response, frequency response, and step response for the causal LTI system satisfying this difference equation?

2.9. (a) First the frequency response:

$$Y(e^{j\omega}) - \frac{5}{6}e^{-j\omega}Y(e^{j\omega}) + \frac{1}{6}e^{-2j\omega}Y(e^{j\omega}) = \frac{1}{3}e^{-2j\omega}X(e^{j\omega})$$

$$\begin{aligned} H(e^{j\omega}) &= \frac{Y(e^{j\omega})}{X(e^{j\omega})} \\ &= \frac{\frac{1}{3}e^{-2j\omega}}{1 - \frac{5}{6}e^{-j\omega} + \frac{1}{6}e^{-2j\omega}} \end{aligned}$$

Now we take the inverse Fourier transform to find the impulse response:

$$\begin{aligned} H(e^{j\omega}) &= \frac{-2}{1 - \frac{1}{3}e^{-j\omega}} + \frac{2}{1 - \frac{1}{2}e^{-j\omega}} \\ h[n] &= -2\left(\frac{1}{3}\right)^n u[n] + 2\left(\frac{1}{2}\right)^n u[n] \end{aligned}$$

For the step response $s[n]$:

$$\begin{aligned} s[n] &= \sum_{k=-\infty}^{\infty} h[k]u[n-k] \\ &= \sum_{k=-\infty}^n h[k] \\ &= -2 \frac{1 - (1/3)^{n+1}}{1 - 1/3} u[n] + 2 \frac{1 - (1/2)^{n+1}}{1 - 1/2} u[n] \\ &= \left(1 + \left(\frac{1}{3}\right)^n - 2\left(\frac{1}{2}\right)^n\right) u[n] \end{aligned}$$

Frequency Response For Rational System Functions

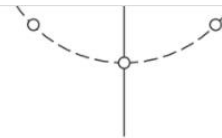


Figure 5.8 Pole-zero plot for Example 5.5.

5.3 FREQUENCY RESPONSE FOR RATIONAL SYSTEM FUNCTIONS

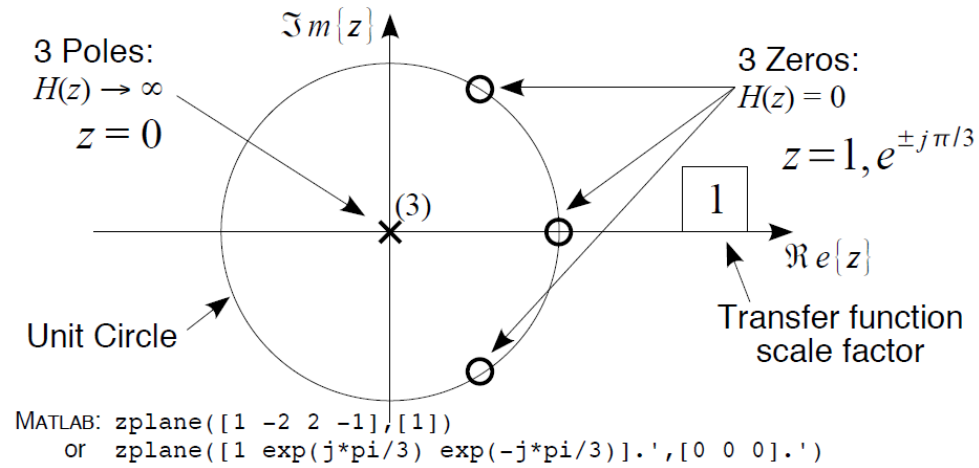
If a stable LTI system has a rational system function, i.e., if its input and output satisfy a difference equation of the form of Eq. (5.19), then its frequency response (the system function of Eq. (5.20) evaluated on the unit circle) has the form

$$H(e^{j\omega}) = \frac{\sum_{k=0}^M b_k e^{-j\omega k}}{\sum_{k=0}^N a_k e^{-j\omega k}}. \quad (5.45)$$

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Poles & Zeros

A pole-zero plot is a useful way of expressing a transfer function. Consider the following for $H(z) = 1 - 2z^{-1} + 2z^{-2} - z^{-3}$.



$$4y[n] = 2y[n-1] - 3y[n-2] + 2x[n] + 3x[n-1] \Rightarrow$$

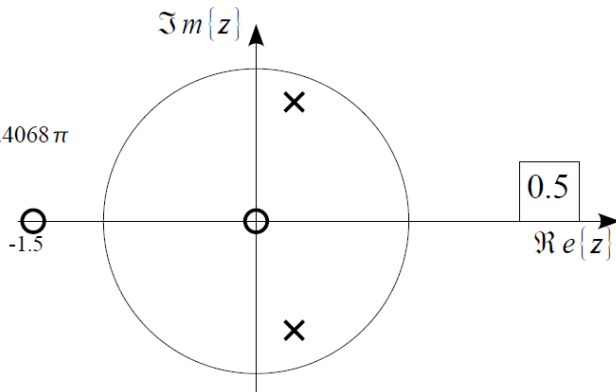
$$H(z) = \frac{2 + 3z^{-1}}{4 - 2z^{-1} + 3z^{-2}}$$

Zeros:

$$z = 0, z = -1.5$$

Poles:

$$z = 0.886e^{\pm j0.4068\pi}$$



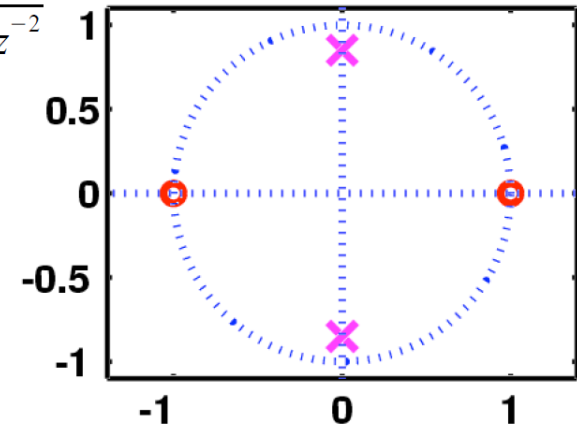
$$H(z) = \frac{1 - z^{-2}}{1 + 0.7225z^{-2}}$$

Zeros:

$$z = \pm 1$$

Poles:

$$z = 0.85e^{\pm j\pi/2}$$



Second Order System

Example (page#296):

Example 5.6 2nd-Order IIR System

Consider the 2nd-order system

$$H(z) = \frac{1}{(1 - re^{j\theta}z^{-1})(1 - re^{-j\theta}z^{-1})} = \frac{1}{1 - 2r \cos\theta z^{-1} + r^2 z^{-2}}.$$

The difference equation satisfied by the input and output of the system is

$$y[n] - 2r \cos\theta y[n - 1] + r^2 y[n - 2] = x[n].$$

Using the partial fraction expansion technique, we can show that the impulse response of a causal system with this system function is

$$h[n] = \frac{r^n \sin[\theta(n + 1)]}{\sin\theta} u[n]. \tag{5.62}$$

The system function in Eq. (5.61) has a pole at $z = re^{j\theta}$ and at the conjugate location, $z = re^{-j\theta}$, and two zeros at $z = 0$. The pole-zero plot is shown in Figure 5.12.

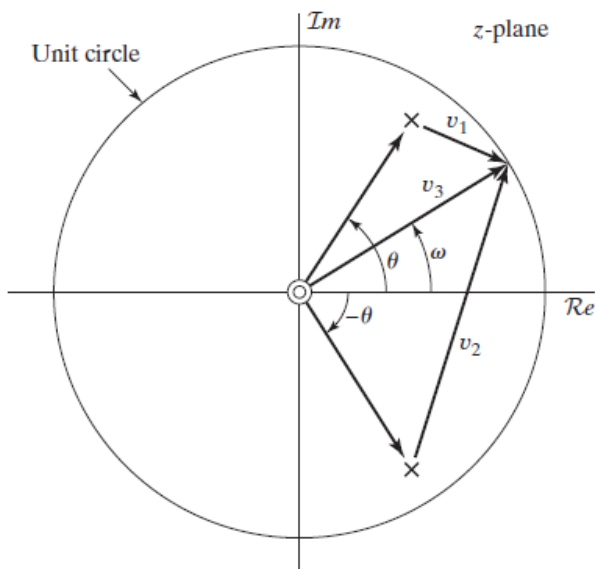


Figure 5.12 Pole-zero plot for Example 5.6.

$$(5.61) \iff H(e^{j\omega}) = \frac{1}{(1 - re^{j\theta}e^{-j\omega})(1 - re^{-j\theta}e^{-j\omega})}$$

$$20 \log_{10} |H(e^{j\omega})| = -10 \log_{10}[1 + r^2 - 2r \cos(\omega - \theta)] - 10 \log_{10}[1 + r^2 - 2r \cos(\omega + \theta)], \tag{5.63a}$$

$$\angle H(e^{j\omega}) = -\arctan\left[\frac{r \sin(\omega - \theta)}{1 - r \cos(\omega - \theta)}\right] - \arctan\left[\frac{r \sin(\omega + \theta)}{1 - r \cos(\omega + \theta)}\right] \tag{5.63b}$$

plotted for $r = 0.9$ and $\theta = \pi/4$.

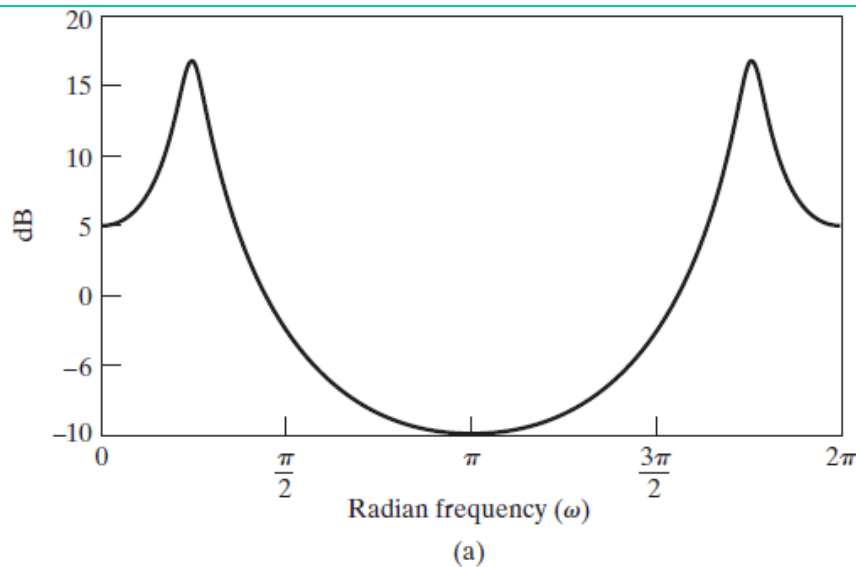


Figure 5.13 Frequency response for a complex-conjugate pair of poles as in Example 5.6, with $r = 0.9$, $\theta = \pi/4$. (a) Log magnitude.

Second Order System (2 poles & 2 zeroes)

$$H(Z) = \frac{(1 - re^{j\omega_0}Z^{-1})(1 - re^{-j\omega_0}Z^{-1})}{(1 - Re^{j\omega_0}Z^{-1})(1 - Re^{-j\omega_0}Z^{-1})} = \frac{1 + b_1Z^{-1} + b_2Z^{-2}}{1 + a_1Z^{-1} + a_2Z^{-2}}$$

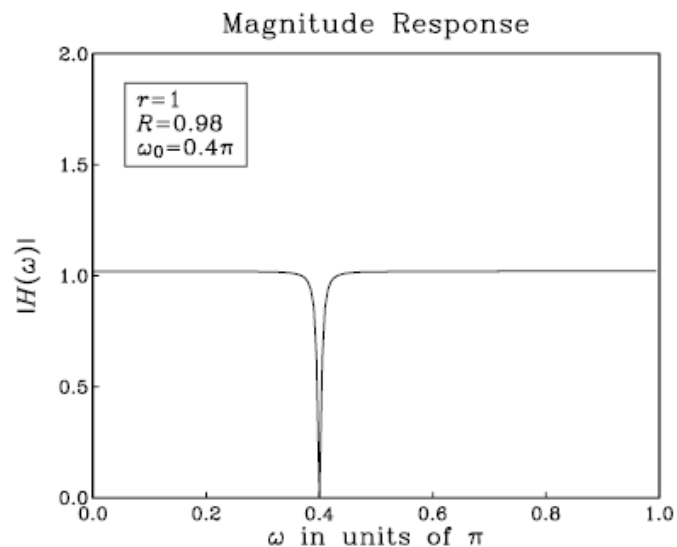
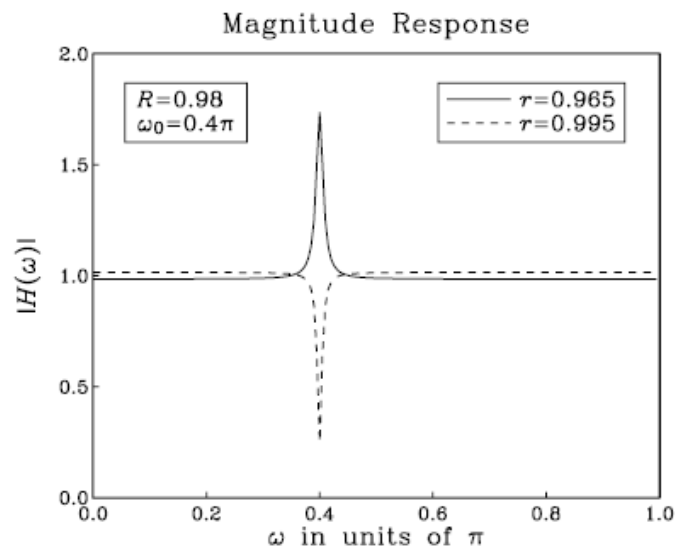
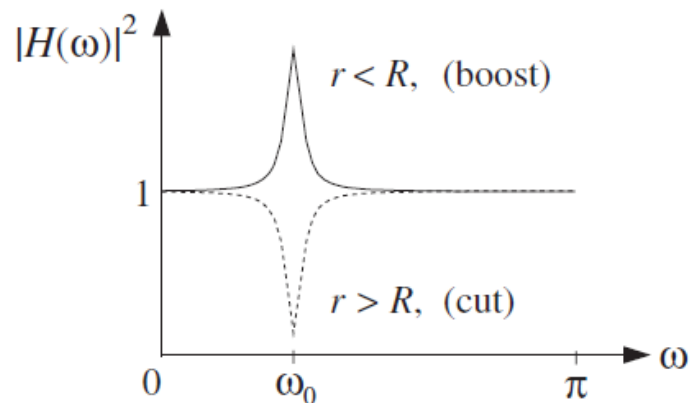
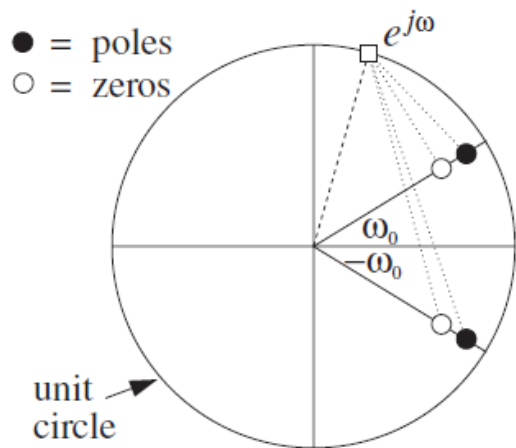
where the filter coefficients are given in terms of the parameters r , R , and ω_0 :

$$\begin{aligned} b_1 &= -2r \cos \omega_0 & b_2 &= r^2 \\ a_1 &= -2R \cos \omega_0 & a_2 &= R^2 \end{aligned}$$

The corresponding magnitude squared response is:

$$|H(e^{j\omega})|^2 = \frac{(1 - 2r \cos(\omega - \omega_0) + r^2)(1 - 2r \cos(\omega + \omega_0) + r^2)}{(1 - 2R \cos(\omega - \omega_0) + R^2)(1 - 2R \cos(\omega + \omega_0) + R^2)}$$

Notch and Comb Filters



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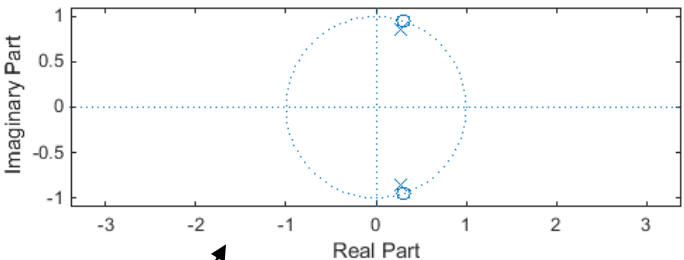
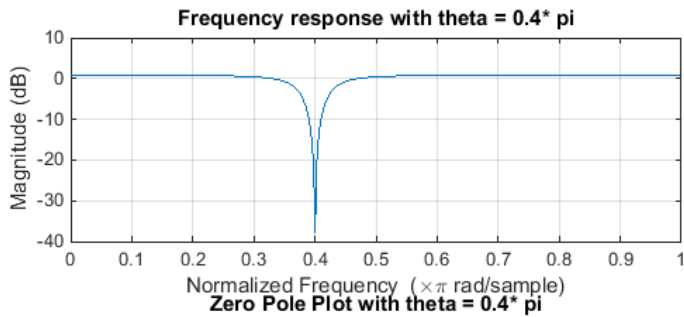
Notch & Comb Filters

Notch filter: If zeros are closer than poles to unit circle

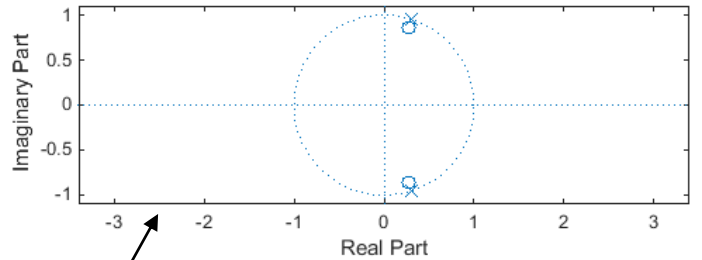
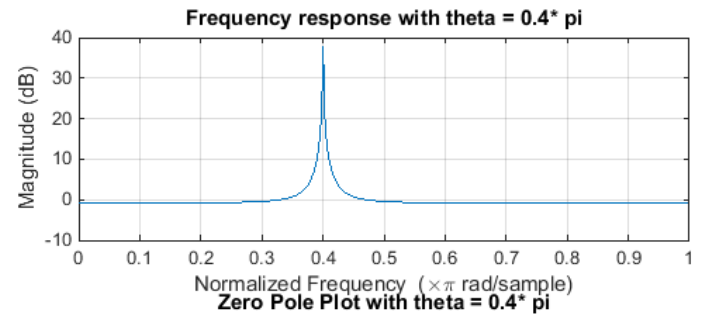
Comb Filter: If poles are closer than zeros to unit circle

$$H(z) = \frac{1 - 2 \cos \theta z^{-1} + z^{-2}}{1 - 1.8 \cos \theta z^{-1} + 0.81z^{-2}}$$

$$H(z) = \frac{1 - 1.8 \cos \theta z^{-1} + 0.81z^{-2}}{1 - 2 \cos \theta z^{-1} + z^{-2}}$$



uOttawa.ca **Notch**



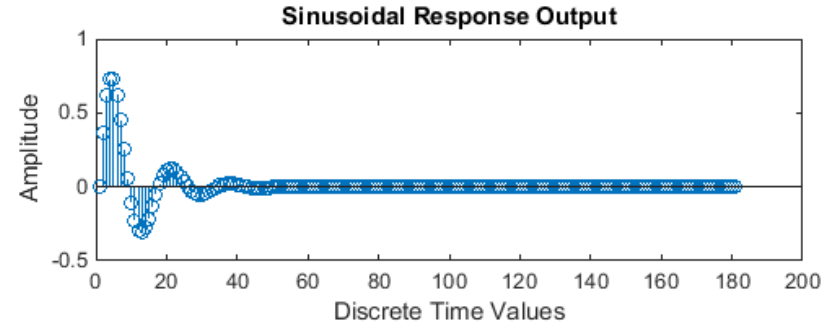
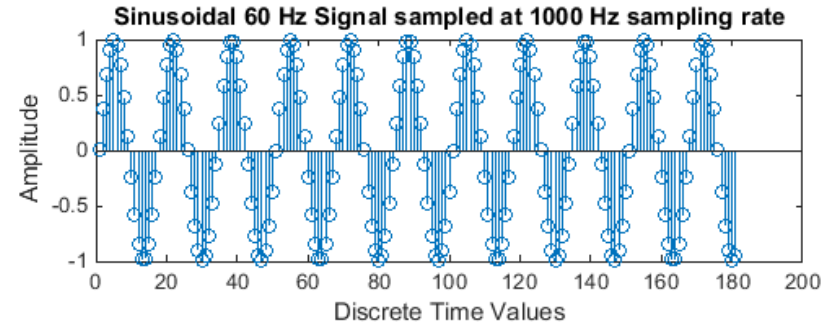
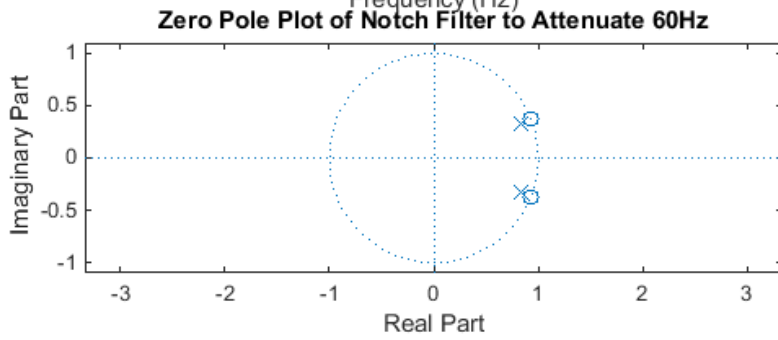
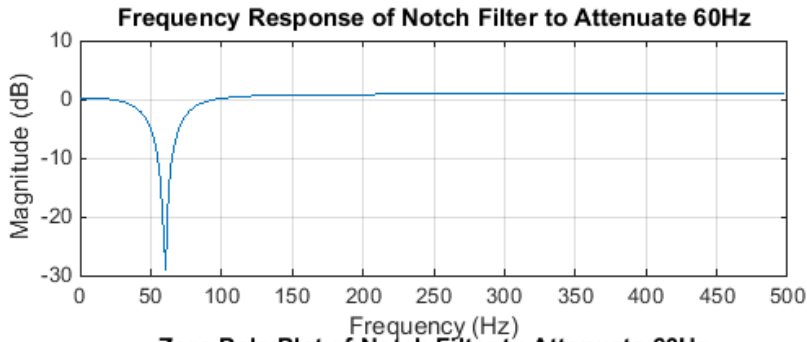
Comb



From Lab2: Remove certain frequency via Notch filter

Removing 60 Hz

$$\theta = \frac{f}{f_s} \cdot 2\pi = 60/1000 \cdot 2\pi$$



Parametric Resonators

As another example, consider the design of a simple second-order “resonator” filter whose frequency response is dominated by a single narrow pole peak at some frequency ω_0 .

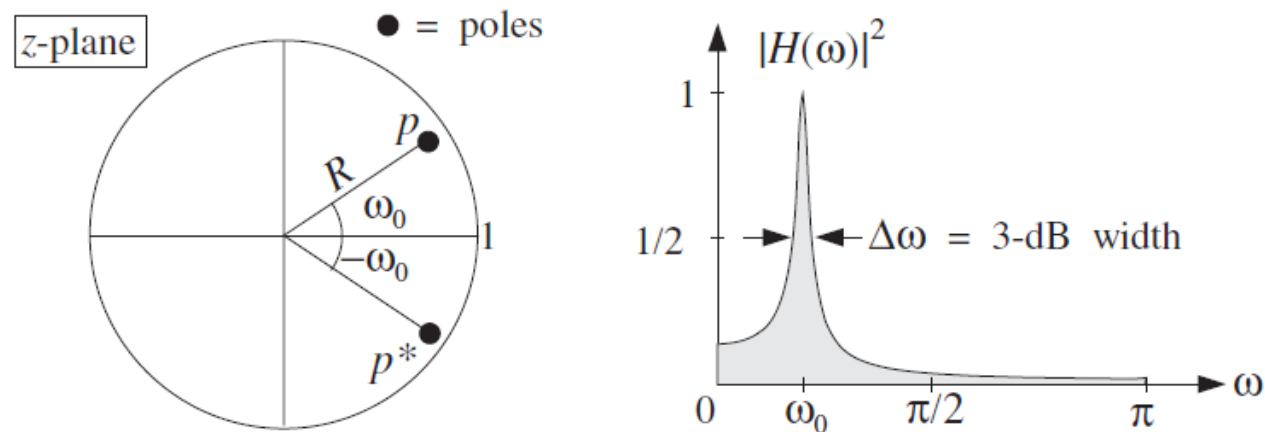


Fig. 6.4.2 Pole/zero pattern and frequency response of resonator filter.

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$$H(z) = \frac{G}{(1 - Re^{j\omega_0}z^{-1})(1 - Re^{-j\omega_0}z^{-1})} = \frac{G}{1 + a_1z^{-1} + a_2z^{-2}} \quad (6.4.3)$$

where a_1 and a_2 are related to R and ω_0 by

$$a_1 = -2R \cos \omega_0, \quad a_2 = R^2$$

The gain G may be fixed so as to normalize the filter to unity at ω_0 , that is, $|H(e^{j\omega})| = 1$. The frequency response of the filter is obtained by the substitution $z = e^{j\omega}$:

$$H(e^{j\omega}) = \frac{G}{(1 - Re^{j\omega_0}e^{-j\omega})(1 - Re^{-j\omega_0}e^{-j\omega})} = \frac{G}{1 + a_1e^{-j\omega} + a_2e^{-2j\omega}}$$

The normalization requirement $|H(\omega_0)| = 1$ gives the condition:

$$|H(\omega_0)| = \frac{G}{|(1 - Re^{j\omega_0}e^{-j\omega_0})(1 - Re^{-j\omega_0}e^{-j\omega_0})|} = 1$$

which can be solved for G :

$$G = (1 - R)\sqrt{1 - 2R \cos(2\omega_0) + R^2}$$

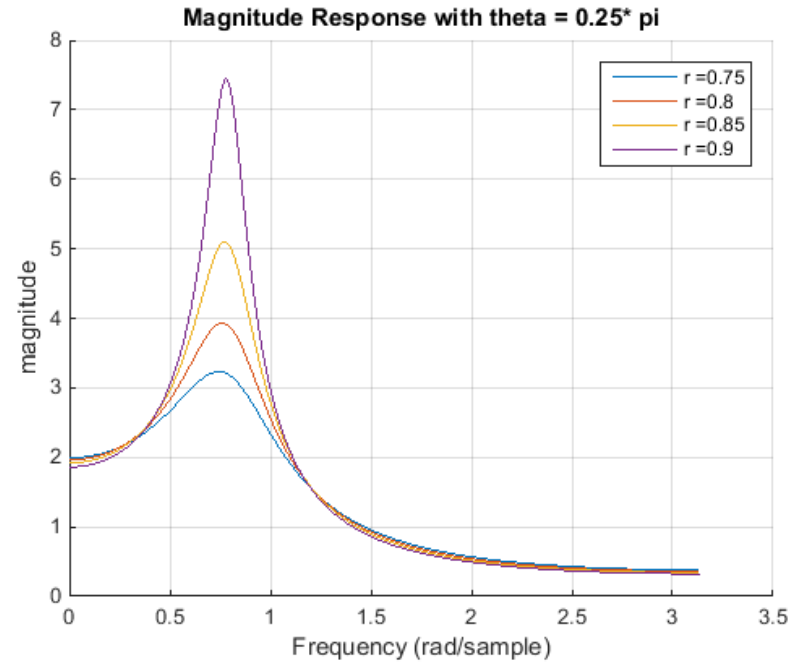
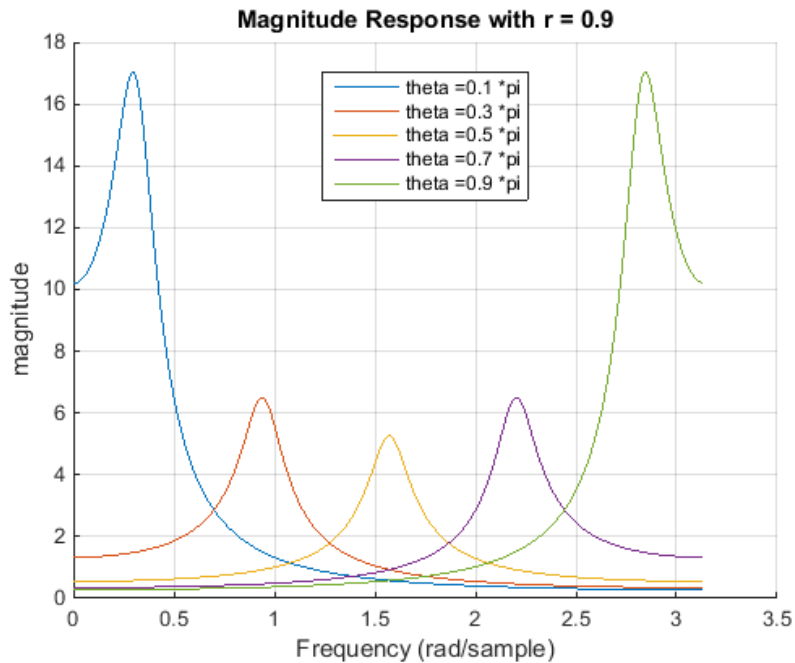


Introduction to Lab#2

FILTERS AND RESONATORS

From Lab2: Resonators

$$H(z) = \frac{1}{1 - 2r \cos \theta z^{-1} + r^2 z^{-2}}$$

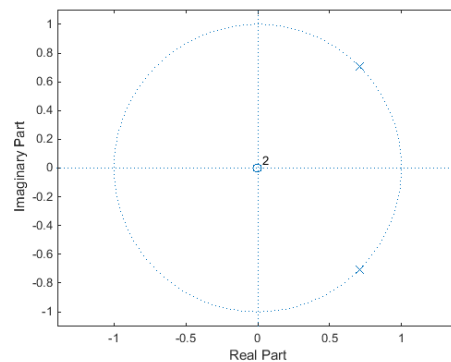
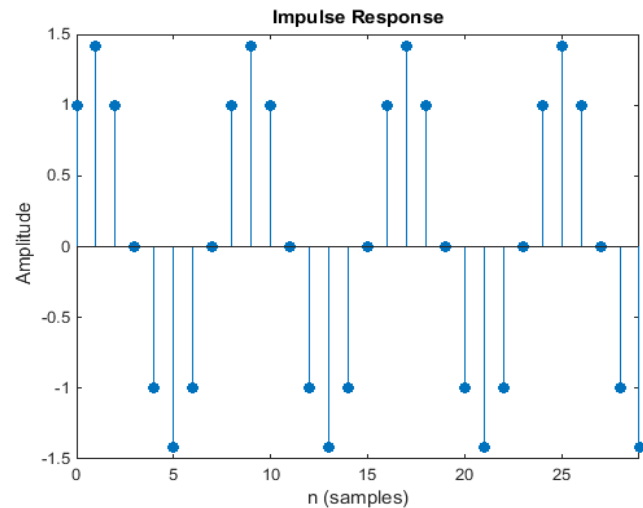
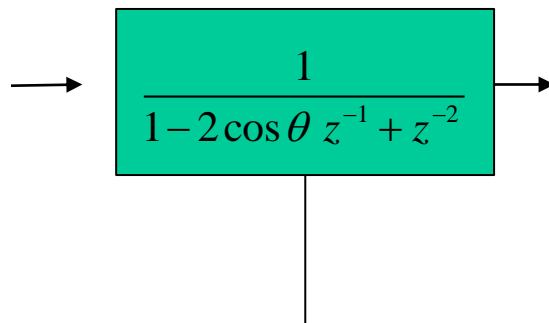
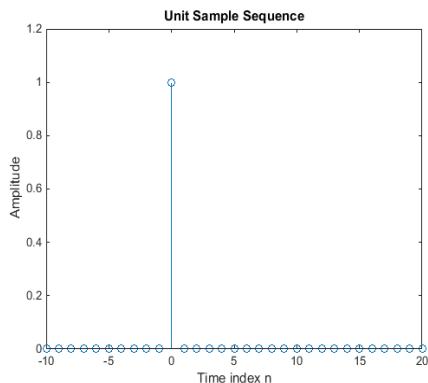


The Gain $G = |H(e^{j\omega})| = \frac{1}{1 - r\sqrt{1 - 2r \cos(2\theta) + r^2}}$

Sinusoid Generator

$$H(z) = \frac{1}{1 - 2r \cos \theta z^{-1} + r^2 z^{-2}}$$

Let $r=1$



$$\text{Frequency} = f = \frac{\theta}{2\pi} \cdot fs$$

THE END