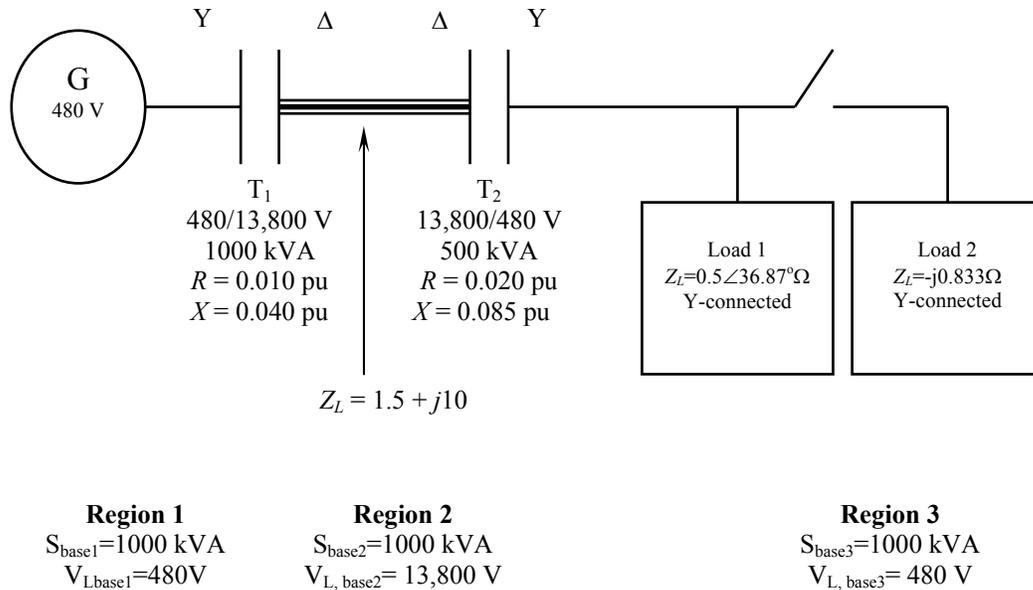


Problem 2-23

The following figure shows a power system consisting of a three-phase 480-V, 60-Hz generator supplying two loads through a transmission line with a pair of transformers at either end.

- Sketch the per-phase equivalent circuit of this power system.
- With the switch open, find the real power P , reactive power Q , and apparent power S supplied by the generator. What is the power factor of the generator?
- With the switch closed, find the real power P , reactive power Q , and apparent power S supplied by the generator. What is the power factor of the generator?
- What are the transmission losses (transformer plus transmission line losses) in this system with the switch open? With the switch closed? What is the effect of adding load 2 to the system?



Solution: This problem can best be solved using the per-unit system of measurements. The power system can be divided into three regions by the two transformers. If the per-unit base quantities in Region 1 are chosen to be $S_{base1} = 1000 \text{ kVA}$ and $V_{L,base1} = 480 \text{ V}$, then the base quantities in Region 2 and 3 will be as shown above. The base impedance of each region will be:

$$Z_{base1} = \frac{3(V\phi_1)^2}{S_{base1}} = \frac{3(277)^2}{1000 \text{ kVA}} = 0.238 \Omega$$

$$Z_{base2} = \frac{3(V\phi_2)^2}{S_{base2}} = \frac{3(7967)^2}{1000 \text{ kVA}} = 190.4 \Omega$$

$$Z_{base3} = \frac{3(V\phi_3)^2}{S_{base3}} = \frac{3(277)^2}{1000 \text{ kVA}} = 0.238 \Omega$$

- a. To have the per-unit, per-phase equivalent circuit, we must convert each impedance in the system to per unit on the base of the region in which it is located. The impedance of transformer T_1 is already in per unit to the proper base

$$R_1, \text{ pu} = 0.010$$

$$X_1, \text{ pu} = 0.040$$

The impedance of transformer T_2 is already in per unit, but it is per-unit to the base of transformer T_2 , so it must be converted to the base of the power system.

$$(R, X, Z)_{\text{pu on base 2}} = (R, X, Z)_{\text{pu on base 1}} \frac{(V_{\text{base1}})^2 (S_{\text{base2}})}{(V_{\text{base2}})^2 (S_{\text{base1}})}$$

$$R_{2,\text{pu}} = 0.02 \frac{(7967 \text{ V})^2 (1000 \text{ kVA})}{(7967)^2 (500 \text{ kVA})} = 0.040$$

$$X_{2,\text{pu}} = 0.085 \frac{(7967 \text{ V})^2 (1000 \text{ kVA})}{(7967)^2 (500 \text{ kVA})} = 0.170$$

The per unit impedance of the transmission line is

$$Z_{\text{line, pu}} = \frac{Z_{\text{line}}}{Z_{\text{base2}}} = \frac{1.5 + j10}{190.4} = 0.00788 + j0.0525$$

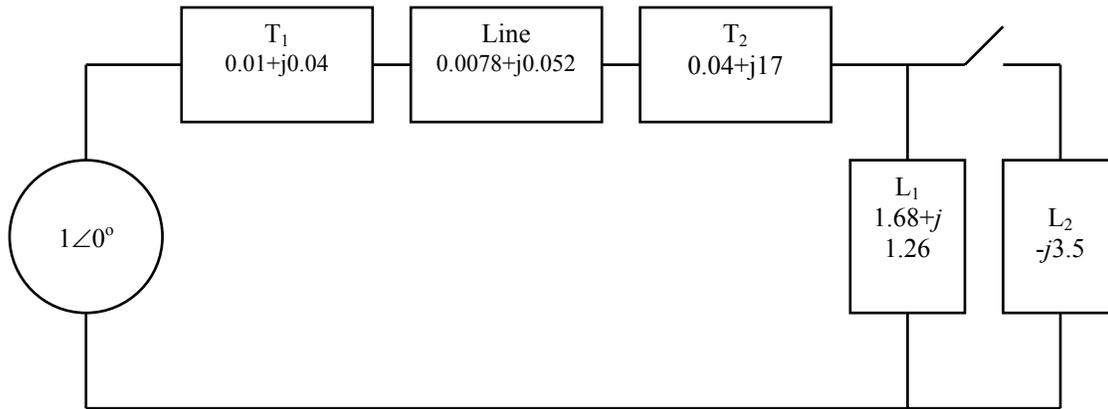
The per unit impedance of load 1 is

$$Z_{\text{load1, pu}} = \frac{Z_{\text{load1}}}{Z_{\text{base3}}} = \frac{0.5 \angle 36.87^\circ}{0.238} = 1.681 + j1.261$$

The per unit impedance of load 2 is

$$Z_{\text{load2, pu}} = \frac{-j0.833}{0.238} = -j3.5$$

The per-unit, per-phase equivalent circuit is shown below



b. With the switch open, the equivalent impedance is

$$Z_T = 0.010 + j0.040 + 0.00788 + j0.0525 + 0.040 + j0.170 + 1.681 + j1.261$$

$$= 2.312 \angle 41.2^\circ$$

The current is

$$I = \frac{1 \angle 0^\circ}{2.312 \angle 41.2^\circ} = 0.4325 \angle -41.2^\circ \text{ A}$$

The load voltage is

$$V_{\text{load, pu}} = I Z_{\text{load}} = (0.4325 \angle -41.2^\circ)(1.681 + j1.261) = 0.909 \angle -4.3^\circ$$

The actual load voltage is $0.909 \times 480 = 436 \text{ V}$.

The power supplied to the load is

$$P_{\text{load, pu}} = I^2 R_{\text{load}} = (0.4325)^2 (1.681) = 0.314$$

$$P_{\text{load}} = P_{\text{load, pu}} S_{\text{base}} = (0.314)(1000 \text{ kVA}) = 314 \text{ kW}$$

The power supplied by the generator

$$P_{G, \text{pu}} = VI \cos \theta = (1)(0.4325) \left(\cos 41.2^\circ \right) = 0.325$$

$$Q_{G, \text{pu}} = VI \sin \theta = (1)(0.4325) \left(\sin 41.2^\circ \right) = 0.285$$

$$S_{G, \text{pu}} = VI = (1)(0.4325) = 0.4325$$

Actual values are: $P_G = 325 \text{ kW}$; $Q_G = 285 \text{ kVAR}$; $S_G = 432.5 \text{ kVA}$

The power factor is: $\cos 41.2^\circ = 0.752$ lagging

c. With the switch closed, the equivalent circuit is

$$Z_T = 0.010 + j0.040 + 0.00788 + j0.0525 + 0.040 + j0.170 + \frac{(1.681 + j1.26)(-j3.5)}{1.681 + j1.261 - j3.5} = 2.698 \angle 5.6^\circ$$

The current is

$$I = \frac{1 \angle 0^\circ}{2.698 \angle 5.6^\circ} = 0.371 \angle -5.6^\circ$$

The load voltage is

$$V_{\text{load, pu}} = I Z_{\text{load}} = (0.371 \angle -5.6^\circ)(2.627 - j0.011) = 0.975 \angle -5.6^\circ$$
$$V_{\text{load}} = (0.975)(480) = 468 \text{ V}$$

The power supplied to the two loads is

$$P_{\text{load, pu}} = I^2 R_{\text{load}} = (0.371)^2 (2.672) = 0.361$$
$$P_{\text{load}} = (0.361)(1000 \text{ kVA}) = 361 \text{ kW}$$

The power supplied by the generator

$$P_{G, \text{pu}} = VI \cos \theta = (1)(0.371) \cos 5.6^\circ = 0.369$$
$$Q_{G, \text{pu}} = VI \sin \theta = (1)(0.371) \sin 5.6^\circ = 0.0369$$
$$S_{G, \text{pu}} = VI = 0.371$$

Multiply each value by 1000 kVA to get actual values: $P_G = 369 \text{ kW}$; $Q_G = 36 \text{ kVAR}$; $S_G = 371 \text{ kVA}$. The power factor of the generator is $\cos 5.6^\circ = 0.995$ lagging.

d. The transmission losses with the switch open are:

$$P_{\text{line, pu}} = (0.4325)^2 (0.00788) = 0.00147$$
$$P_{\text{line}} = (0.00147)(1000) = 1.47 \text{ kW}$$

The transmission losses with the switch closed are

$$P_{\text{line, pu}} = (0.371)^2 (0.00788) = 0.00108$$
$$P_{\text{line}} = (0.00108)(1000) = 1.08 \text{ kW}$$

Load 2 improved the power factor of the system.